Schoolof
Engineering

## FEM and Elasticity Theory Gebril $\mathfrak{E l - F a l l a h ~}$

EG3111 - Finite $\mathcal{E l}$ ement Analysis and Design

## 2b. A FEM for elasticity based on energy

- As for any PDE, the equations of elasticity can be solved using Weighted Residual Methods, as introduced in section 1b.
- However, the equations of elasticity can also be solved using a physical model, and this approach is always used to formulate the elastic FEM.
- In this physical method, an expression for the total energy of the system, $\Pi$, is determined.
- The displacement field is selected such that it minimises the total energy, e.g., if the DOF is $c$ then the solution satisfies

$$
\frac{\partial \Pi}{\partial c}=0
$$

## 2b. A FEM for elasticity based on energy

The energy of an elastically deformed body consists of two parts such that

$$
\Pi=U+\Omega
$$

Where:
$U$ is known as the elastic stored energy or the elastic strain energy
$\Omega$ is the potential energy of the applied loads

## 2b. Elastic strain energy, $U$



The factor of a half appears as the force increases with the displacement.

## 2b. Elastic strain energy density, w

$$
\begin{aligned}
& w=\frac{\text { Force }}{\text { Area }} \times \frac{\text { Displacement }}{\text { Length }} \\
& =\text { stress } \times \text { strain } \\
& =\text { area under the curve } \\
& =\frac{1}{2} \sigma_{x} \epsilon_{x}
\end{aligned}
$$

Total strain energy:

$$
U=\int_{V} w d V=\frac{1}{2} \int_{V} \sigma_{x} \epsilon_{x} d V
$$

Volume of the body

Typically the stress and strain (and hence $w$ ) vary throughout the body

## 2b. Potential energy of the applied loads

## Two types of contributions.

I. The potential energy of the load $\boldsymbol{P}$ (traction applied to the external end surface) is given by

$$
\boldsymbol{\Omega}=-\boldsymbol{P} \boldsymbol{u}_{\boldsymbol{L}}
$$

Where $u_{L}$ is the distance moved by the applied load $P$.
(The minus sign shows that work is done by the load)
ii. The potential energy of the body force (force per unit volume)

$$
\boldsymbol{\Omega}=-\int_{\boldsymbol{V}} f_{x} u d \boldsymbol{v}
$$

(You can show that this is the change in total potential energy mgh of the body before and after loading).

2b. (i) Simple 1D extension using FEM


Cross-sectional area, $A$

$$
\Pi=U+\Omega
$$

Where

$$
\begin{gathered}
U=\int_{V} w d V=\frac{1}{2} \int_{V} \sigma_{x} \epsilon_{x} d V \\
\Omega=-P u_{L} \\
\Omega=-\int_{V}^{\text {or }} f_{x} u d V
\end{gathered}
$$

## 2b. (i) Simple 1D extension using FEM



Young's modulus, $E$
Cross-sectional area, $A$
Propose a linear shape function for the solution

$$
\begin{gathered}
u(x)=u_{L}\left(\frac{x}{L}\right) \\
u(0)=0
\end{gathered}
$$

$$
u(L)=u_{L} \quad \text { Our DOF to be determined }
$$

One DOF is end displacement $u_{L}$

## 2b. (i) Simple 1D extension using FEM

Elastic strain energy

$$
U=\frac{1}{2} \int_{V} \sigma_{x} \epsilon_{x} d V
$$

$$
\begin{gathered}
\epsilon_{x}=\frac{d u}{d x}=\frac{u_{L}}{L} \quad V=A L \\
U=\frac{1}{2} \int_{V} \sigma_{x} \epsilon_{x} d V=\frac{1}{2} A \int_{0}^{L} E \epsilon_{x}^{2} d x=\frac{1}{2} E A \int_{0}^{L} \epsilon_{x}^{2} d x \\
U=\frac{1}{2} E A \int_{0}^{L}\left(\frac{u_{L}}{L}\right)^{2} d x \quad \begin{array}{l}
\text { The elastic strain energy is } \\
\text { always a second order } \\
\text { polynomial in terms of DOF }
\end{array} \\
U=\frac{1}{2} \frac{E A u_{L}^{2}}{L^{2}} L=\frac{1}{2} \frac{E A}{L} u_{L}^{2} \quad
\end{gathered}
$$

## 2b. (i) Simple 1D extension using FEM



Cross-sectional area, $A$

Potential energy of the applied load


## 2b. (i) Simple 1D extension using FEM

Total energy

$$
\Pi=\frac{1}{2} \frac{E A}{L} u_{L}^{2}-P u_{L} \quad E q 4
$$

Minimize total energy with respect to DOF
Differentiate Eq 4

$$
\frac{\partial \Pi}{\partial u_{L}}=0 \quad \Longrightarrow \quad \frac{E A}{L} \mathrm{u}_{\mathrm{L}}-\mathrm{P}=0
$$

Same result as before Because the proposed shape function has the same form as the exact solution.

$$
\Longrightarrow \mathrm{u}_{\mathrm{L}}=\frac{\mathrm{PL}}{\mathrm{EA}} \quad \Longrightarrow \quad u(x)=\frac{\mathrm{P}}{\mathrm{EA}} \mathrm{x}
$$

## 2b. (ii) Self-weight using FEM



Try solving this problem using:
I. Linear (1 DOF: $u_{1}$ ) shape function

$$
u(x)=u_{1}\left(\frac{x}{L}\right)
$$

ii. Quadratic (2 DOF: $a$ and $b$ ) shape function

$$
u(x)=a\left(\frac{x}{L}\right)+b\left(\frac{x}{L}\right)^{2}
$$

## 2b. (ii) Self-weight (Linear Shape Function)

$$
\prod_{x}
$$

$$
\begin{gathered}
f_{x}=\rho g \\
U=\frac{1}{2} E A \int_{0}^{L} \epsilon_{x}^{2} d x
\end{gathered}
$$

Propose

$$
\begin{gathered}
u(x)=u_{1}\left(\frac{x}{L}\right) \\
U=\frac{1}{2} E A \int_{0}^{L}\left(\frac{u_{1}}{L}\right)^{2} d x=\frac{1}{2} \frac{E A}{L} u_{1}^{2} \\
\Omega=-\int_{V} f_{x} u(x) d V=-\int_{0}^{L} \rho g \cdot u_{1}\left(\frac{x}{L}\right) A d x=-\frac{\rho g \cdot u_{1} \cdot A}{L} \int_{0}^{L} x d x \\
=-\frac{1}{2} A \rho g L \cdot u_{1}
\end{gathered}
$$

## 2b. (ii) Self-weight (Linear Shape Function)



Next section... (3) Bar Elements

