

FEM and Elasticity Theory

Gebríl El-Fallah

EG3111 – Fíníte Element Analysis and Design



2b. A FEM for elasticity based on energy

- As for any PDE, the equations of elasticity can be solved using Weighted Residual Methods, as introduced in section 1b.
- However, the equations of elasticity can also be solved using a physical model, and this approach is always used to formulate the elastic FEM.
- In this physical method, an expression for the total energy of the system, Π, is determined.
- The displacement field is selected such that it minimises the total energy, *e.g.*, if the DOF is *c* then the solution satisfies

$$\frac{\partial \Pi}{\partial c} = 0$$



2b. A FEM for elasticity based on energy

The energy of an elastically deformed body consists of two parts such that

$$\Pi = U + \Omega$$

Where:

U is known as the elastic stored energy or the elastic strain energy

 $\boldsymbol{\Omega}$ is the potential energy of the applied loads



2b. Elastic strain energy, U



The factor of a half appears as the force increases with the displacement.



2b. Elastic strain energy density, w

Torsion spring



Total strain energy:

$$U = \int_{V} w \, dV = \frac{1}{2} \int_{V} \sigma_x \epsilon_x dV$$

Volume of the body

Typically the stress and strain (and hence *w*) vary throughout the body



2b. Potential energy of the applied loads

Two types of contributions.

I. The **potential energy of the load** *P* (traction applied to the external end surface) is given by

 $\Omega = -Pu_L$

Where u_L is the distance moved by the applied load *P*. (The minus sign shows that work is done by the load)

ii. The potential energy of the body force (force per unit volume)

$$\Omega = -\int_V f_x u \, dV$$

(You can show that this is the change in total potential energy mgh of the body before and after loading).





Propose a linear shape function for the solution

$$u(x) = u_L \left(\frac{x}{L}\right)$$
$$u(0) = 0$$
$$u(L) = u_L$$
 Our DOF to be determined

One DOF is end displacement u_L



$$U = \frac{1}{2} \int_{V} \sigma_{x} \epsilon_{x} dV$$

Elastic strain energy

$$\epsilon_x = \frac{du}{dx} = \frac{u_L}{L} \qquad \qquad V = AL$$

$$U = \frac{1}{2} \int_{V} \sigma_{x} \epsilon_{x} \, dV = \frac{1}{2} A \int_{0}^{L} E \epsilon_{x}^{2} \, dx = \frac{1}{2} E A \int_{0}^{L} \epsilon_{x}^{2} \, dx$$

$$U = \frac{1}{2} EA \int_0^L \left(\frac{u_L}{L}\right)^2 dx$$

 $U = \frac{1}{2} \frac{EAu_L^2}{L^2} L = \frac{1}{2} \frac{EA}{L} u_L^2 \checkmark$

The elastic strain energy is always a second order polynomial in terms of DOF





Potential energy of the applied load





Total energy

$$\Pi = \frac{1}{2} \frac{EA}{L} u_L^2 - P u_L \qquad \qquad Eq \ 4$$

Minimize total energy with respect to DOF

Differentiate Eq 4

$$\frac{\partial \Pi}{\partial u_L} = 0 \quad \Longrightarrow \quad \frac{EA}{L} u_L - P = 0$$

Same result as before.... Because the proposed shape function has the same form as the exact solution.

$$\implies$$
 $u_L = \frac{PL}{EA} \implies u(x) = \frac{P}{EA}x$



2b. (ii) Self-weight using FEM

Try solving this problem using:

I. Linear (1 DOF: u_1) shape function $u(x) = u_1 \left(\frac{x}{L}\right)$

ii. Quadratic (2 DOF: *a* and *b*) shape function $u(x) = a\left(\frac{x}{L}\right) + b\left(\frac{x}{L}\right)^2$



 u_I

 \mathbf{V}_{x}

2b. (ii) Self-weight (Linear Shape Function)

$$u(x) = u_{1}\left(\frac{x}{L}\right) \qquad f_{x} = \rho g$$

$$U = \frac{1}{2}EA \int_{0}^{L} \epsilon_{x}^{2} dx$$
Propose
$$u(x) = u_{1}\left(\frac{x}{L}\right)$$

$$U = \frac{1}{2}EA \int_{0}^{L} \left(\frac{u_{1}}{L}\right)^{2} dx = \frac{1}{2}\frac{EA}{L}u_{1}^{2}$$

$$u_{L} \qquad \Omega = -\int_{V} f_{x}u(x)dV = -\int_{0}^{L} \rho g. u_{1}\left(\frac{x}{L}\right) Adx = -\frac{\rho g. u_{1}.A}{L} \int_{0}^{L} x dx$$

$$= -\frac{1}{2}A\rho gL. u_{1}$$

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2b. (ii) Self-weight (Linear Shape Function)

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Next section... (3) Bar Elements

